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PATENT
KEL01 P-133

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Applicant : Ian Hill
Serial No. : 10/821,542
Filed : April 9, 2004
For : LOCKING MECHANISM FOR A LINEAR ACTUATOR

Commissioner for Patents
P.O. Box 1450
Alexandria VA 22313-1450

Dear Sir:

CERTIFICATE OF MAIL

I certify that the attached return postcard, Claim of Priority, and a certified copy of United Kingdom Patent Application No. 0308409.2 are being deposited with the United States Postal Service as first class mail in an envelope addressed to:

Commissioner for Patents
P.O. Box 1450
Alexandria VA 22313-1450

on June 9, 2004.

Catherine S. Collins
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Enclosures

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P.O. Box 1450
Alexandria VA 22313-1450

Dear Sir:

CLAIM OF PRIORITY

Applicant hereby claims the priority benefits under the provisions of 35 U.S.C. 119, basing said claim of priority on United Kingdom patent Application No. 0308409.2, filed April 22, 2003.

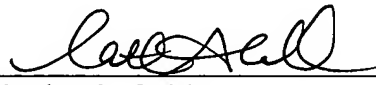
In accordance with the provisions of 35 U.S.C. 119 and 37 C.F.R. 1.55(a), a certified copy of the above listed United Kingdom patent application is attached.

Respectfully submitted,

IAN HILL

By: Van Dyke, Gardner, Linn & Burkhardt, LLP

Dated: June 9, 2004


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INVESTOR IN PEOPLE

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IAN HILL

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Patents ADP number (if you know it)

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8609273001

4. Title of the invention

LOCKING MECHANISM FOR A LINEAR ACTUATOR

5. Name of your agent (if you have one)

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I/We request the grant of a patent on the basis of this application.

Signature



Date

11/4/03

ALAN WALLACE, AGENT FOR APPLICANT

12. Name and daytime telephone number of person to contact in the United Kingdom

ALAN WALLACE 02890 236000

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LOCKING MECHANISM FOR A LINEAR ACTUATOR

The present invention relates to linear actuators and in particular to a locking mechanism for use therewith.

- 5 The invention is particularly, but not exclusively, suited for use with hydraulic linear actuators.

Hydraulic linear actuators are well known and are often referred to as hydraulic cylinders or hydraulic rams.

- 10 In some applications failure of the actuator or its associated pipework, or accidental operation by an operator can result in personal injury or damaged equipment. Hydraulic check valves can be used to safeguard against pipework failure but such check
15 valves do not protect against a piston, seal or other failure internal to the actuator.

- It is known to provide an additional mechanical locking device which may be either manually or automatically
20 operable. If the locking device is manually operated, then its operation relies upon the operator correctly inserting the locking device. A simple prop as used under the raised body of a tipper type lorry is an example of a manually inserted locking device.

- 25 Automatic locking devices often require extra control devices and actuators and this results in size and cost penalties. An example of an automatic locking device is the 'scotch' lever used on vertically stroking hydraulic presses. Whichever conventional approach is
30 adopted, it can be rendered useless by either human error or mechanical/electrical failure.

It is considered therefore that there is a need for an improved locking mechanism for linear actuators.

Accordingly a first aspect of the invention provides a locking mechanism for a linear actuator comprising a piston rod arranged for linear movement between a fully retracted state and a fully extended state, the locking mechanism comprising a piston follower coupled to the piston rod for movement therewith, and a latching member moveable between a non-locked state and at least one locked state in which the latching member obstructs the movement of the piston follower such that the piston rod is prevented from adopting the fully retracted state.

Preferably, the latching member is pivotable with respect to the actuator. Preferably, the latching member is biased to adopt a locked state. For example, a spring, or other biasing means, may be provided between the latching member and the actuator. The latching member may comprise one or more latching bars pivotably mounted on, or coupled to, the actuator. In the illustrated embodiment, the latching member comprises two spaced-apart latching bars, each being pivotably coupled to a respective opposite side of the actuator.

Preferably, the latching member includes one or more bearing surfaces for engagement with the piston follower. Advantageously, the latching member includes a plurality of bearing surfaces, each arranged to engage with the piston follower, or a respective part thereof, in a respective locked state, wherein the location of each bearing surface in the respective locked state is arranged to halt the movement of the

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piston rod at a respective state of extension between the fully extended and fully retracted states. In the illustrated embodiment, each latching bar is shaped to define a plurality of respective bearing surfaces.

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Preferably, the latching member includes one or more catching surfaces for engagement with the piston follower, as the latching member moves towards the, or a respective locked state, so that the, or a
10 respective, bearing surface is held in the path of the piston follower. In the preferred embodiment, the or each bearing surface is associated with a respective catching surface. Advantageously, the or each bearing surface is substantially perpendicular with its
15 respective catching surface. This may be arranged by providing a respective substantially L-shaped recess in the latching member.

Preferably, the piston follower is arranged for
20 corresponding linear movement with the piston rod. In the preferred embodiment, the piston follower comprises one or more bar, or rod, which is substantially parallel with the piston rod. In the illustrated embodiment, the piston follower comprises two spaced-
25 apart rods located adjacent respective opposite sides of the actuator and arranged for engagement with a respective latching bar. Advantageously, a guide or support member may be provided for guiding the movement of the piston follower (or parts thereof) and provided
30 support thereto (or to parts thereof).

In the preferred embodiment, the locking mechanism further includes one or more secondary actuators

arranged to actuate the latching member, or a respective part thereof, from the at least one locked state to the non-locked state. Advantageously, the actuator (main actuator) and the or each secondary
5 actuator are inter-linked so that they may each be operated by a common operating circuit, e.g. hydraulic circuit. Preferably, the common operating circuit is operable in a first mode, in which the piston rod of main actuator is caused to extend, a second mode, in
10 which the piston rod of the main actuator is caused to retract and the respective piston rods of the or each secondary actuator may extend, or a third mode, in which the respective piston rods of both the main and secondary actuators extend.

15

In the preferred embodiment, the main actuator is a double acting actuator having a piston chamber divided into a retract side and an extend side, the retract side being inter-linked with the secondary actuator(s)
20 so that operating fluid may be supplied to the secondary actuator(s) from said retract side to cause the respective piston rods of the secondary actuator(s) to extend. In this arrangement, said third mode of operation is effected by supplying operating fluid,
25 under pressure, to both sides of the main actuator simultaneously.

Other advantageous aspects and features of the invention will be apparent to those ordinarily skilled
30 in the art upon review of the following description of a specific embodiment of the invention and with reference to the accompanying drawings.

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Embodiments of the invention are now described by way of example and with reference to the accompanying drawings in which like numerals are used to indicate like parts and in which:

5

Figure 1 is a perspective view of a hydraulic linear actuator including a first embodiment of a locking mechanism according to the invention;

- 10 Figure 2 is a perspective view of a hydraulic linear actuator including a second embodiment of a locking mechanism according to the invention;

- Figure 3 is an alternative perspective view of the
15 hydraulic linear actuator and locking mechanism of Figure 2;

- Figure 4 is a perspective view of a hydraulic linear actuator including a third embodiment of a locking
20 mechanism according to the invention;

- Figure 5 is an alternative perspective view of the hydraulic linear actuator and locking mechanism of Figure 4;

25

Figure 6 is a further alternative perspective view of the hydraulic linear actuator and locking mechanism shown in Figures 2 and 3;

- 30 Figure 7 is a table illustrating the operation of a valve switch suitable for use by the locking mechanisms of Figures 1 to 6; and

6

Figure 8 is a schematic of a hydraulic circuit suitable for use by the locking mechanisms of Figures 1 to 6.

Referring now to Figure 1 of the drawings, there is shown, generally indicated as 10, a hydraulic linear actuator comprising a piston chamber 12, piston 14 (not visible in Figure 1 but shown schematically in Figure 8) and piston rod 16. In the example of Figure 1, a rod eye 18 is provided at the free external end of the piston rod 18 for connecting the rod 18 to an article (not shown) that requires actuation by the actuator 10. It will be understood that a variety of alternative conventional connectors may be used in place of the rod eye 18.

15

The actuator 10 is generally conventional in its configuration and operation. The piston rod 18 is linearly actuatable between a fully retracted state, in which the piston rod 16 is retracted within the piston chamber 12 to a maximum extent, and a fully extended state in which the piston rod 16 extends from the piston chamber 12 to a maximum extent. In Figure 1 the piston rod 16 is shown in an intermediate state between the fully extended and fully retracted states. The state of the piston rod 16 is controlled by the flow of hydraulic fluid, usually oil, into and out of the piston chamber 12. For use with the preferred embodiments described hereinafter, the actuator 10 is assumed to be a double-acting actuator in which the state of the piston rod 16 is controlled by the flow of hydraulic fluid into and out of two fluid inlet/outlet ports (not shown in Figure 1), wherein the piston 14 is located between the two ports.

Hydraulic actuators of the type described above are commonly referred to as hydraulic cylinders (because the piston chamber 12 is usually generally cylindrical as shown in Figure 1) or hydraulic rams.

Figure 1 also illustrates a first embodiment of a locking mechanism according to the invention. The locking mechanism is comprised of two main components, namely a piston follower 20 and a latch assembly 22.

The piston follower 20 comprises a rod or bar (or any other suitable member) which coupled to the piston rod 16 for movement therewith. At least a portion of the piston follower 20 is located externally of the piston chamber 12 so that it may be engaged by the latch assembly as is described in more detail below. In the embodiment of Figure 1, the piston follower 20 comprises two rods 21, 21' each of which is connected to, or adjacent, the free end of piston rod 16 so that the rods 21, 21' are substantially parallel with the piston rod 16. This may be achieved, by way of example, by means of a connecting bar or plate 24 which also, conveniently, may carry the rod eye 18.

When the piston rod 16 moves linearly between the fully retracted and fully extended states, or between any of the infinite number of intermediate states therebetween, the piston follower 20 moves linearly by a corresponding amount in the same direction. Each of the rods 21, 21' has a respective free end 26, 26' (only one visible in Figure 1) located externally of

the piston cylinder 12 for engagement with the latching assembly 22.

Advantageously, a guide or support member may be
5 provided for guiding the movement of the piston
follower 20. In Figure 1, a guide member in the form
of a plate 28 is carried by the exterior of the piston
cylinder 12 and is shaped to define a respective
aperture or channel through which the respective rods
10 21, 21' pass. The plate 28 helps to reduce flexing or
bending of rods 21, 21' which may occur when under
load.

It will be understood that, in alternative embodiments
15 (not illustrated) the piston follower may comprise only
one, or more than two, rods or other follower members.

The latching assembly 22 comprises one or more latch
members 30 comprising at least one respective bearing
20 surface for engagement with the piston follower 20 in
order to limit the piston follower's linear travel. In
the Figure 1 embodiment, the latching assembly
comprises a latch member 30 having two substantially
parallel latching bars 31, 31' each comprising a
25 respective bearing surface 32, 32'.

The latching bars 31, 31' are operatable between a non-
locked state (as shown in Figure 1) in which the
latching bars 31, 31' do not interfere with the
30 movement of the piston follower 20, and a locked state
(shown in Figures 2 and 5), in which the latching bars
31, 31', and in particular the respective bearing
surfaces 32, 32', obstruct the movement of the piston

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follower 20 thereby preventing the piston rod 16 from reaching its fully retracted state.

Preferably, the latching member 30 is pivotable with respect to the piston cylinder 12. In Figure 1, the latching bars 31, 31' are pivotably mounted, at respective pivot points 33, 33', on a butt member 34 located at the base of the piston cylinder 12 (i.e. the end of the cylinder opposite that from which the piston rod 16 extends). The latching bars 31, 31' are therefore pivotable between the non-locked state and the locked state about their respective pivot points 33, 33'.

In the preferred embodiment, the latching member 30 is biased towards the locked state. In the embodiment of Figure 1, a respective spring 36, 36' (only one visible in Figure 1) is provided between each latching bar 31, 31' and the butt 34 and is arranged to urge the respective latching bar 31, 31' into the locked state. It will be understood that other conventional biasing means (not illustrated) may alternatively be used for this purpose and that the biasing means need not necessarily be connected to the butt 34 as long as it acts on the latching member 30 in the manner described. Moreover, in the embodiment of Figure 1, the latching bars 31, 31' are joined together by a cross bar 40 such that their movement is unitary. In such an embodiment, there is no need to provide a respective biasing spring, or the like, for each latching bar 31, 31'.

In an alternative embodiment (not illustrated), the latching member is arranged to be urged towards the

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locked state under the influence of gravity and no biasing is required.

The latching member 30 is arranged so that the latching
5 bars 31, 31' are disposed at opposite sides of the
piston chamber 12 and are arranged for engagement with
a respective rod 21, 21' of the piston follower when in
the locked state. Each latching bar 31, 31' is shaped
to define a catching surface 38, 38' for engaging with
10 the piston follower 20 as the latching member 30 moves
into the locked state thereby halting the movement of
the latching member 30 so that the respective bearing
surface 32, 32' is located in the path of the
respective rod 21, 21'. Preferably, the bearing
15 surface 32, 32' and its respective catching surface 38,
38' are substantially perpendicular to one another and
are provided by a substantially L-shaped recess formed
in the respective latching bar 31, 31'.

20 In use, when the piston rod is in the fully retracted
state, the latching member 30 is prevented from
adopting the locked state by the piston follower 20 (as
shown in Figure 1). As the piston rod 16 is extended
towards the fully extended state, the piston follower
25 20 moves clear of the latching member 30 thereby
allowing it to adopt the locked state under the action
of the springs 36, 36'. In the locked state, the
catching surfaces 38, 38' engage against the respective
rods 21, 21' thereby positioning the respective bearing
30 surfaces 32, 32' in the respective path of the free
ends 26, 26' of the respective rods 21, 21'. This may
best be appreciated from Figure 5. It will be seen
that the piston rod 16 is prevented from returning to

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the fully retracted state since the movement of the piston follower 20 is obstructed by the latching member 30, and in particular the bearing surfaces 32, 32'. Hence, in the locked state, the latching member 30 restricts, or limits, the movement of the piston rod 16.

Figures 2, 3 and 6 show an alternative embodiment which is generally similar to the embodiment of Figure 1 and in which like numerals are used to indicate like parts. In Figures 2, 3 and 6, for illustration purposes only, the latching bars 131, 131' are not interconnected. Further, each latching bar 131, 131' is shaped to define more than one bearing surface 132, 132' and more than one catching surface 138, 138'. This allows the latching mechanism 130 to adopt more than one locked state. Preferably, each bearing surface 132, 132' has a respective associated catching surface 138, 138' which, advantageously, are substantially perpendicular to one another. In Figures 2 and 3, prefixes A and B are used to denote associated bearing and catching surfaces. Associated bearing and catching surfaces 132, 132', 138, 138' may be defined by respective substantially L-shaped recesses formed in the respective latching bars 131, 131'. From an alternative viewpoint, the bearing and catching surfaces 132, 132', 138, 138' may be formed by providing the latching bars 131, 131' with a serrated or toothed edge.

30

Hence, the latching member 130 adopts one of a plurality of locked states in sequence depending on the extension of the piston rod 16. In each progressive

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locked state, a respective bearing surface 132, 132' prevents the respective rods 21, 21' from retracting further than a respective intermediate state, the respective intermediate states being progressively

5 further away from the fully retracted state. Hence, the location of the in use bearing surface 132, 132' in the path of the rods 20, 20' varies depending on the extension of the piston rod 16. This restricts the amount by which the piston rod 16 can retract in the

10 event of failure. The amount by which the piston rod 16 can retract in the event of failure is effectively determined by the length of the catching surfaces 138, 138'.

15 By way of example and with reference to Figure 2, the latching bar 131' is shown in a first locked state in which catching surface A138' engages with the free end 26' of rod 21' thereby holding bearing surface A132' in the path of rod 21'. The travel of rod 21' in a

20 direction towards the fully retracted state is thus restricted - the piston rod 16 would be prevented from reaching the fully retracted state by engagement of the end 26' of rod 21' and the bearing surface A132'. As the piston rod 16 extends towards the fully extended

25 state, the end 26' of rod 21' moves clear of catching surface A138'. Latching bar 131' then pivots about pivot point 33', under the action of spring 36', until catching surface B138' engages with rod 21' thereby holding bearing surface B132' in the path of rod 21'.

30 Hence, the latching bar 131' adopts a second locked state (not illustrated) in which the travel of piston rod 16 is further restricted in that, when the end 26' of rod 21' engages with bearing surface B132', the

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piston rod 16 is held further from the fully retracted state that it is in the first locked state. Similarly, as the piston rod 16 extends still further, the latching bar 131' adopts a third locked state in which bearing surface C132' is located in the path of rod 21'. In the third locked state the travel of piston rod 16 is still further restricted in that, when the end 26' of rod 21' engages with bearing surface C132', the piston rod 16 is held still further from the fully retracted state.

It will be seen, therefore, that as the piston rod 16 extends, the location of the in use bearing surface 132' varies between locked states such that the piston 16 is prevented from travelling towards the fully retracted state past a respective intermediate state which is progressively further from the fully retracted state. In the illustrated embodiments, this is achieved by arranging the latching bar 131' such that the respective distance between the respective bearing surfaces A132', B132', C132' and pivot point 33' increases.

Hence, the latching member 30, 130 automatically adopts a locked state as the piston rod 16 extends. In the event of hydraulic or other failure, the piston rod 16 the travel of the piston rod 16 towards the fully retracted state is restricted by the latching member 30, 130.

In one embodiment (not illustrated) the latching member 30, 130 may be returned to the non-locked state manually. Preferably, however, one or more release

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actuators, and in particular, hydraulic actuators are provided for this purpose.

5 In Figure 1, the latching member 30 is unitary (since latching bars 31, 31' are mechanically interconnected by cross bar 40) and so one release actuator 42 is provided. The release actuator 42 is arranged to act on the latching member 30, conveniently on cross bar 40, such that extension of the actuator 42 moves the
10 latching member 30 to the non-locked state. The release actuator 42 is preferably a linear hydraulic actuator and may be the same general type as actuator 10, although dual ports are not required.

15 Figures 4 and 5 show an alternative embodiment exhibiting features of both the embodiments of Figure 1 and of Figures 2 and 3. The embodiment of Figures 4 and 5 is generally similar to the embodiments already described and similar numerals are used to indicate
20 like parts. In Figures 4 and 5, the latching member 130 has a serrated or toothed end similar to that of the Figure 2, 3 and 6 embodiment, although the latching bars 131, 131' are mechanically interconnected by a cross bar 40 similarly to the embodiment of Figure 1.
25 Hence, a single release actuator 42 may also be used in the embodiment of Figures 4 and 5. In the embodiment of Figures 2, 3 and 6, a respective release actuator 42, 42' is provided for each latching bar 131, 131'.

30 The, or each, hydraulic actuator 42, 42' is advantageously operable by a hydraulic circuit (not shown in Figures 1 to 6) which is integral with the

15

hydraulic circuit (not shown in Figures 1 to 6) used to operate the main actuator 10.

A suitable hydraulic circuit 50 for operating the main
5 actuator 10 and the, or each, release actuator 42, 42'
is shown schematically in Figure 8. The circuit 50
includes a hydraulic fluid (typically oil) source 52
and sink 54. The circuit further includes valve
switches SV1, SV2 for controlling the flow of hydraulic
10 fluid to and from the hydraulic actuators 10, 42, 42'.

Hydraulic actuator 10 is shown schematically in Figure
8 and includes two fluid ports P1, P2 by which
hydraulic fluid may flow into and out of the piston
15 chamber 12 via fluid lines 56, 58. The chamber 12 is
divided into two sections, S1 ("extend side") and S2
("retract side"), by the piston 14. Fluid flow into P1
causes a build up of fluid pressure in section S1 of
the chamber 12 and this exerts a force on piston 14
20 which causes piston rod 16 to extend. As the piston 14
extends, fluid flows out of P2. Similarly, fluid flow
into P2 causes a build up of fluid pressure in section
S2 of the chamber 12 and this exerts a force on piston
14 which causes piston rod 16 to retract.

25

A schematic representation of the, or each, release
actuator 42, 42' is also shown in Figure 8 (only one
shown). The actuator 42, 42' has a fluid port P3 by
which hydraulic fluid may flow into and out of the
30 piston chamber 44 via fluid line 60. Fluid flow into
P3 causes a build up of fluid pressure behind the
piston 48 (i.e. on the side of the piston 48 opposite
the piston rod 46) and this exerts a force on piston 48

which causes piston rod 46 to extend. Unlike the main actuator 10, actuators 42, 42' are not (at least in the illustrated embodiment) double acting actuators.

Retraction of the piston rod 46 may therefore be effected by any suitable means. For example, after a reduction in fluid pressure behind the piston 48 by an outflow of hydraulic fluid from port P3, piston rod 46 may be retracted under the influence of gravity (depending on the in use orientation of the actuator 42, 42'), and/or under the action of the latching member 30, 130 as it adopts the locked state, and/or under the action of a return mechanism (not shown) such as a spring.

In the preferred embodiment port P3 is fed from, or in fluid communication with, the forward, or retract side (section S2) of chamber 12 (i.e. the side of chamber 12 fed by P2). Hence, a build up of fluid pressure in section S2 of chamber 12 causes fluid to be supplied to chamber 44 via P3. This causes a build up of pressure behind piston 48 which, in turn, causes piston rod 46 to extend. When piston rod 16 retracts, piston rod 46 is caused to extend provided there is a sufficient build up of fluid pressure in section S2 to cause fluid to be fed to the chamber 44.

The respective states of valves SV1, SV2 are controllable by a switch mechanism (not shown) which may adopt one of three switch states. These are illustrated in Figure 7 as states A, B and C. In state A, SV1 is open to allow fluid to be supplied into piston chamber 12 via port P1. SV2 is closed to prevent fluid from being fed to P2, but allows fluid to

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flow from P2 and to return to the sink 54. Hence, in switch state A, piston rod 16 extends.

In switch state A, the piston rod 16 extends in normal manner and, as piston rod 16 extends, the latching member 30, 130 will adopt a locking state as described above. When it is desired to retract the piston rod 16, and assuming that no failure has occurred (i.e. that the rods 21, 21' are not in engagement with the bearing surfaces 32, 32', 132, 132'), the switch mechanism is operated to cause the valves SV1, SV2 to adopt switch state C.

In switch state C, SV2 is open to allow fluid to be supplied into piston chamber 12 via port P2. SV1 is closed to prevent fluid from being fed to P1, but allows fluid to flow from P1 and to return to the sink 54. Hence, in switch state C, piston rod 16 retracts. Also, because chambers 12, 44 are interconnected, fluid flow into chamber 12 via port 2 results in fluid flow into chamber 44 via port 3. As a result, piston rod 46 extends. The extension of piston rod 46 causes the respective actuator 42, 42' to move the latching member 30, 130 to the non-locked state. The arrangement is such that, in this normal mode of operation, the, or each, actuator 42, 42' has moved the latching member 30, 130 into the non-locked state before the piston follower 20 would have otherwise engaged with one or more bearing surfaces 32, 32', 132, 132'. Hence, the latching member 30, 130 is moved to the non-locked state before or during retraction of the piston rod 16 and does not interfere with the retraction of the piston rod 16.

However, should a failure occur such that the piston follower 20 is in engagement with one or more bearing surfaces 32, 32', 132, 132', then such engagement prevents, or inhibits, the latching member 30, 130 from moving to the non-locked state in the manner described above. It is therefore preferred to cause the main piston rod 16 to extend slightly to disengage the piston follower 20 from the latching member 30, 130.

10

In the preferred embodiment, this is achieved by causing the switch mechanism to adopt switch state B. In switch state B, both valves SV1, SV2 are open to allow fluid to be supplied to both sides of piston chamber 12 via both ports P1, P2. Hydraulic fluid is supplied to both sides of piston chamber 12 simultaneously and at substantially the same pressure. This results in a net out-stroke (extension) of piston rod 16 due to differential piston sizes (the force exerted on piston 14 from section S1 will be greater than the force exerted on piston 14 from section S2. This is because the surface area of piston 14 on which fluid in section S2 can act is smaller than the surface area of piston 14 on which fluid in section S1 can act (because of the piston rod 16)). This has the effect of disengaging the piston follower 20 and the latching member 30, 130.

The pressure of fluid supplied to P2 is sufficiently high to ensure that fluid is simultaneously fed to chamber 44 via port 3 and this causes the, or each, piston rod 46 to extend thereby moving the latching member 30, 130 to the non-locked state. The switching

mechanism may then be returned to state C to allow the piston rod 16 to be retracted normally.

5 The provision of switch state B and the corresponding operation of the hydraulic circuit 50 and actuators 10, 42, 42' is advantageous in that it ensures that the piston follower 20 does not become jammed against the latching bars 31, 31', 131, 131' thereby preventing the latch member 30, 130 from being moves to the non-locked
10 state. This can occur as a result of a "race" between the retracting piston rod 16 and the extending piston rod 48: in order to extend the piston rod 48 fluid pressure must be built up in section S2 of piston chamber 12. However, should the resultant force
15 exerted on piston 14 be tending to retract piston rod 16, sufficient pressure may not be built up until the actuator 10 encounters a stop, which could take the form of engagement between piston follower 20 and the latching bars 31, 31', 131, 131'.

20 The switching mechanism may be manually operatable or automatically operable as is convenient. In either case, in the preferred embodiment, to disengage the piston follower from the latching member, state B is
25 adopted (typically for a few seconds) followed by state C to retract the piston rod 16.

It will be appreciated from the foregoing that the locking mechanism described herein provides an
30 automatic locked state which substantially prevents any significant unwanted retraction of the main piston rod 16 as a result of any failure of the main actuator 10.

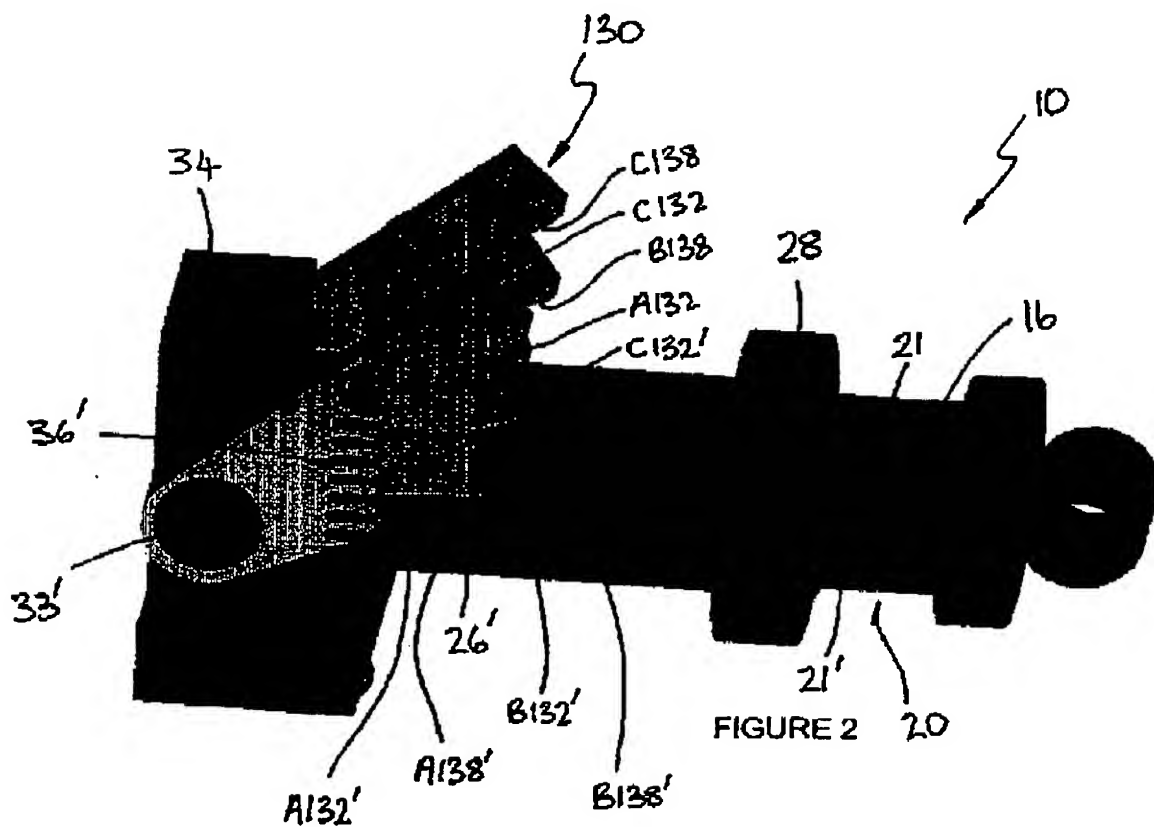
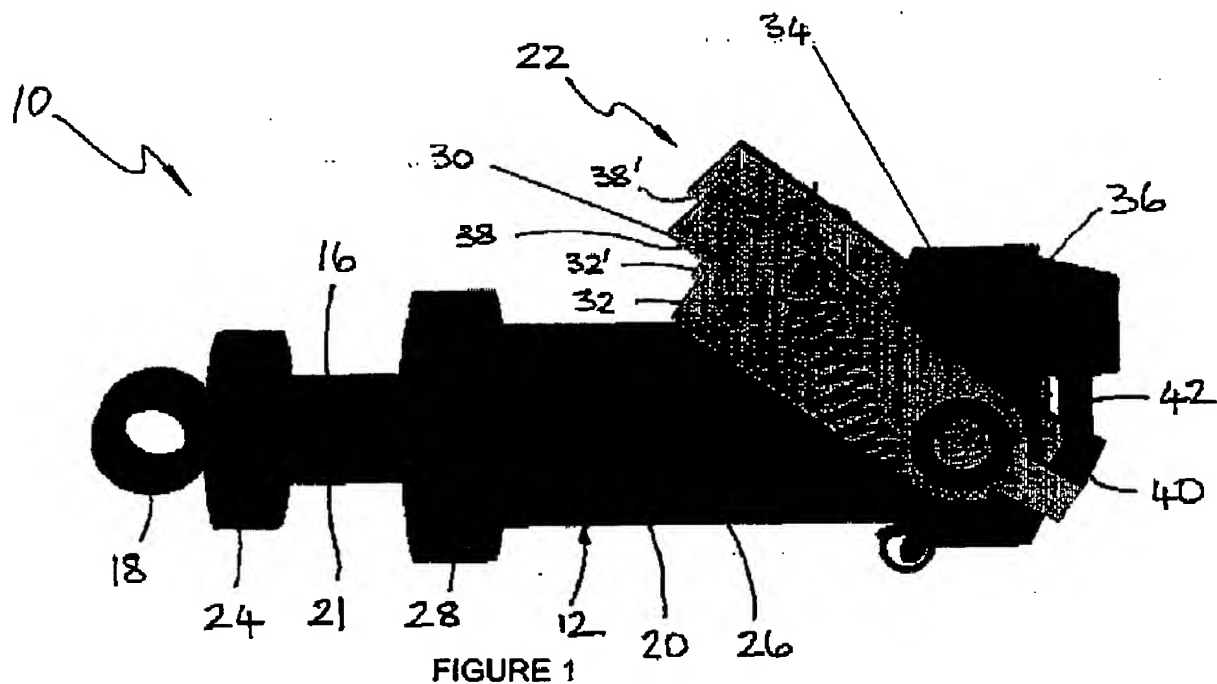
Moreover, the locking mechanism may not readily be moved to the non-locked state through operator error.

A further advantage of the preferred embodiment is that the additional actuator(s) 42, 42' and associated hydraulic circuitry required to release the latching member 30, 130 do not cause significant penalties in terms of cost and size. The locking mechanism and main actuator 10 may be formed as an integral unit, sharing a common hydraulic circuit (which may be housed in the butt 34 and or chamber 12 body) and requires no additional hydraulic connections or components other than would be required by a conventional hydraulic actuator. Hence the actuator 10 with the locking mechanism of the invention may be used as a direct replacement for conventional actuators.

The invention is described herein in the context of a double acting, dual port hydraulic actuator. It will be understood, however, that at least some aspects of the invention may also be used with non-hydraulic actuators, e.g. spring-biased actuators, or with single port and/or single acting actuators. Further, alternative hydraulic fluid supply arrangements for actuators 10, 42, 42' other than that depicted in Figure 8 may be employed.

The invention is not limited to the embodiments described herein which may be modified or varied without departing from the scope of the invention.

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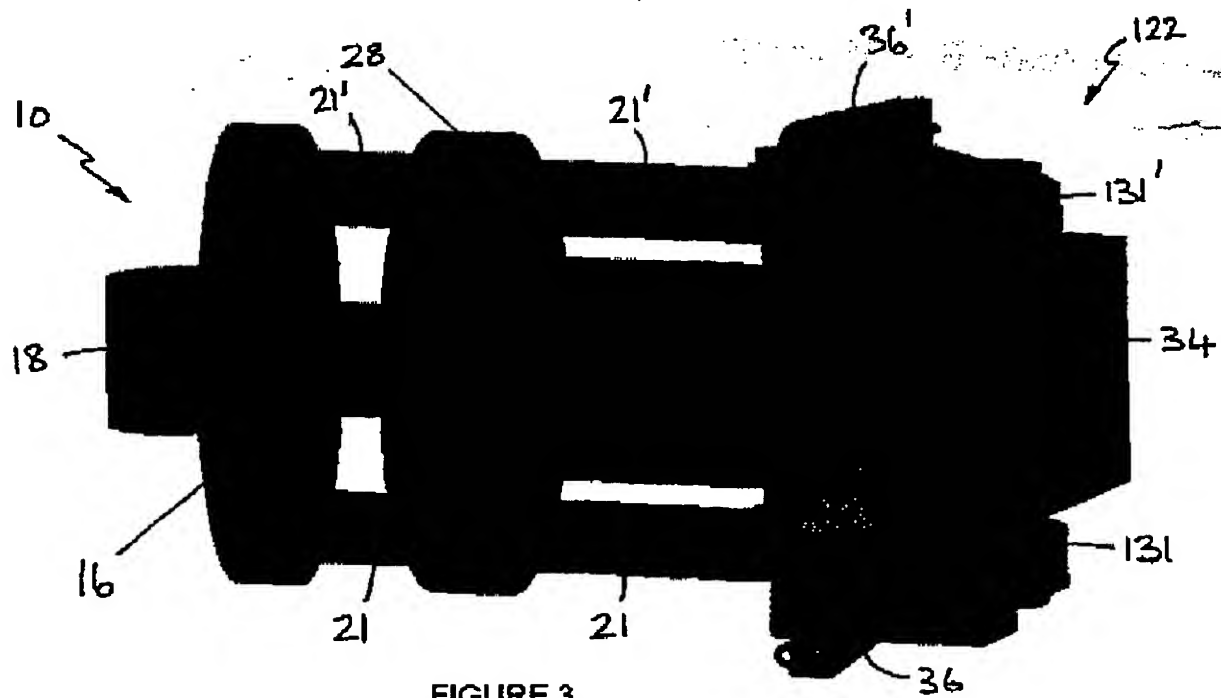


FIGURE 3

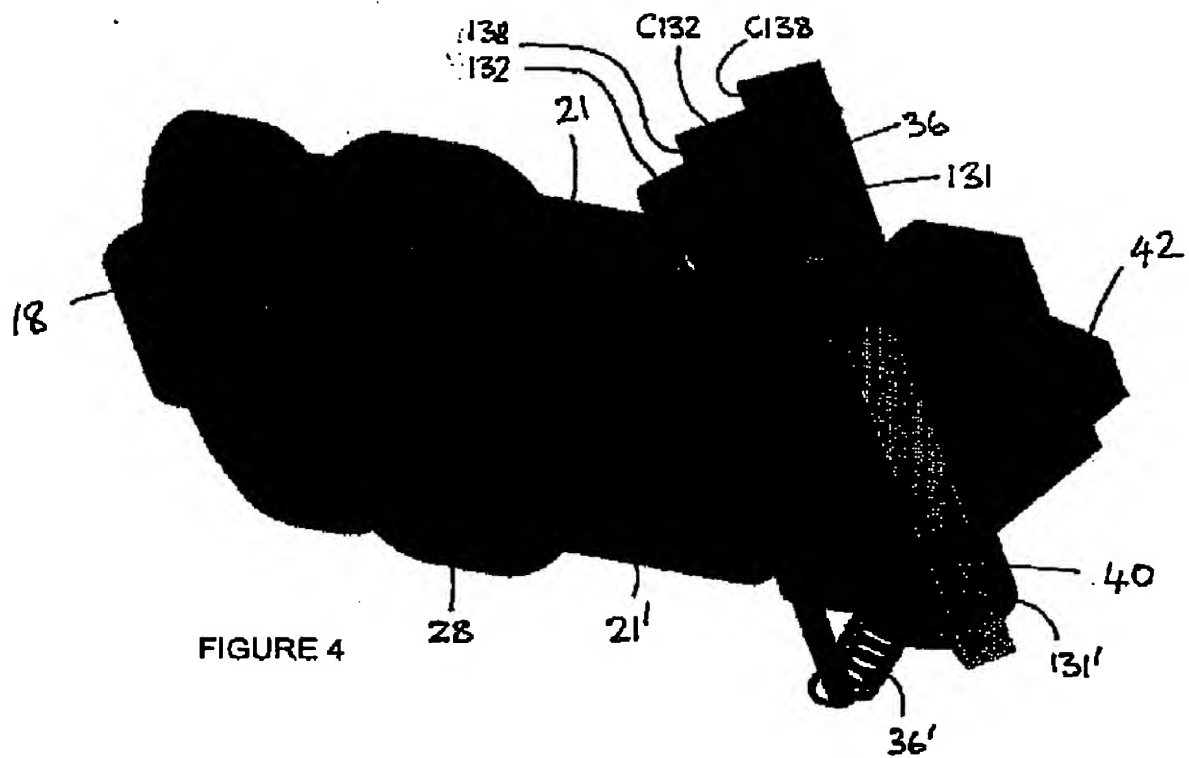
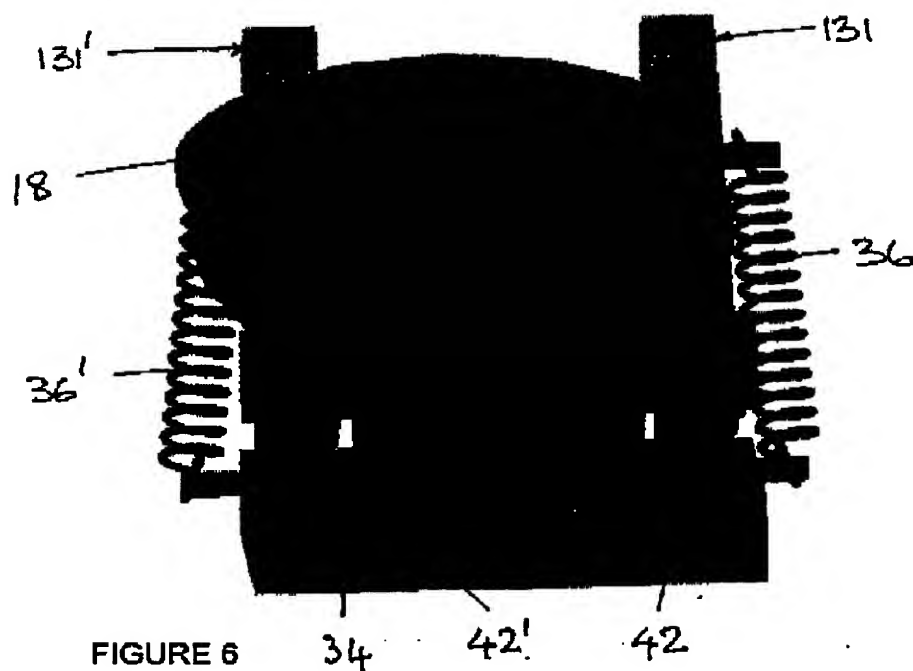
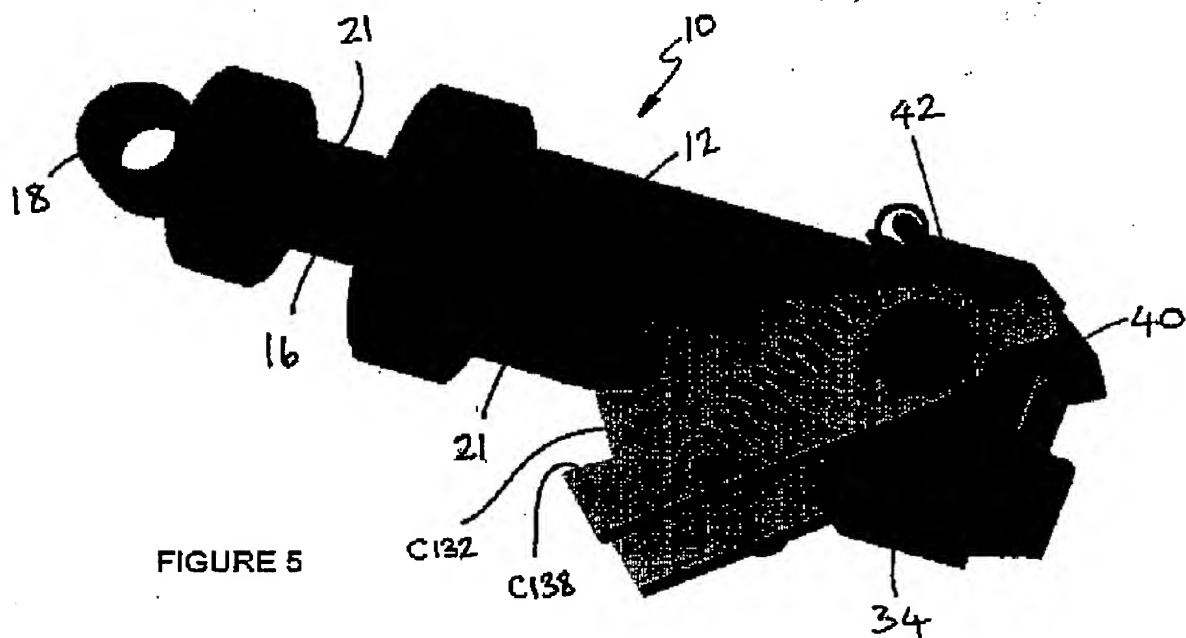


FIGURE 4

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